

# **650 MHz coupler, couple of new ideas**

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## Power requirements for 650 MHz coupler:

Project-X requirements:  $\approx 18 \text{ MV} \times 1 \text{ mA} + \text{overhead} + \text{safety margin} \approx 30 \text{ kW}$

Project -X, 5 mA upgrade:  $\sim 100 \text{ kW}$

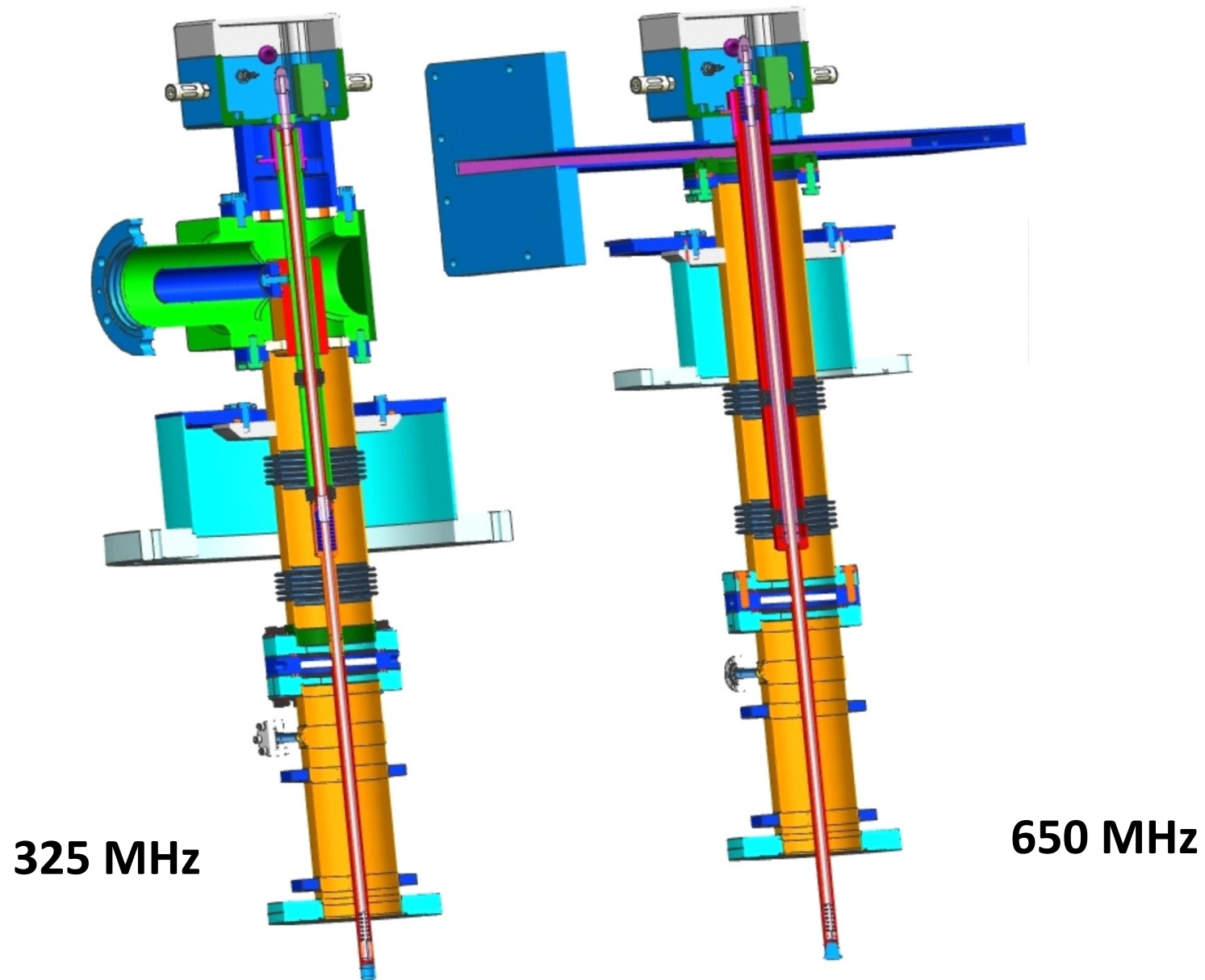
PIP – II:  $\approx (18 \text{ MV} \times 2 \text{ mA} + \text{overhead} + \text{safety margin}) \times \text{duty factor} \approx$   
 $\approx 50 \text{ kW} \times 0.01 \approx 0.5 \text{ kW}$

PIP – II CW upgrade:  $\approx 50 \text{ kW}$

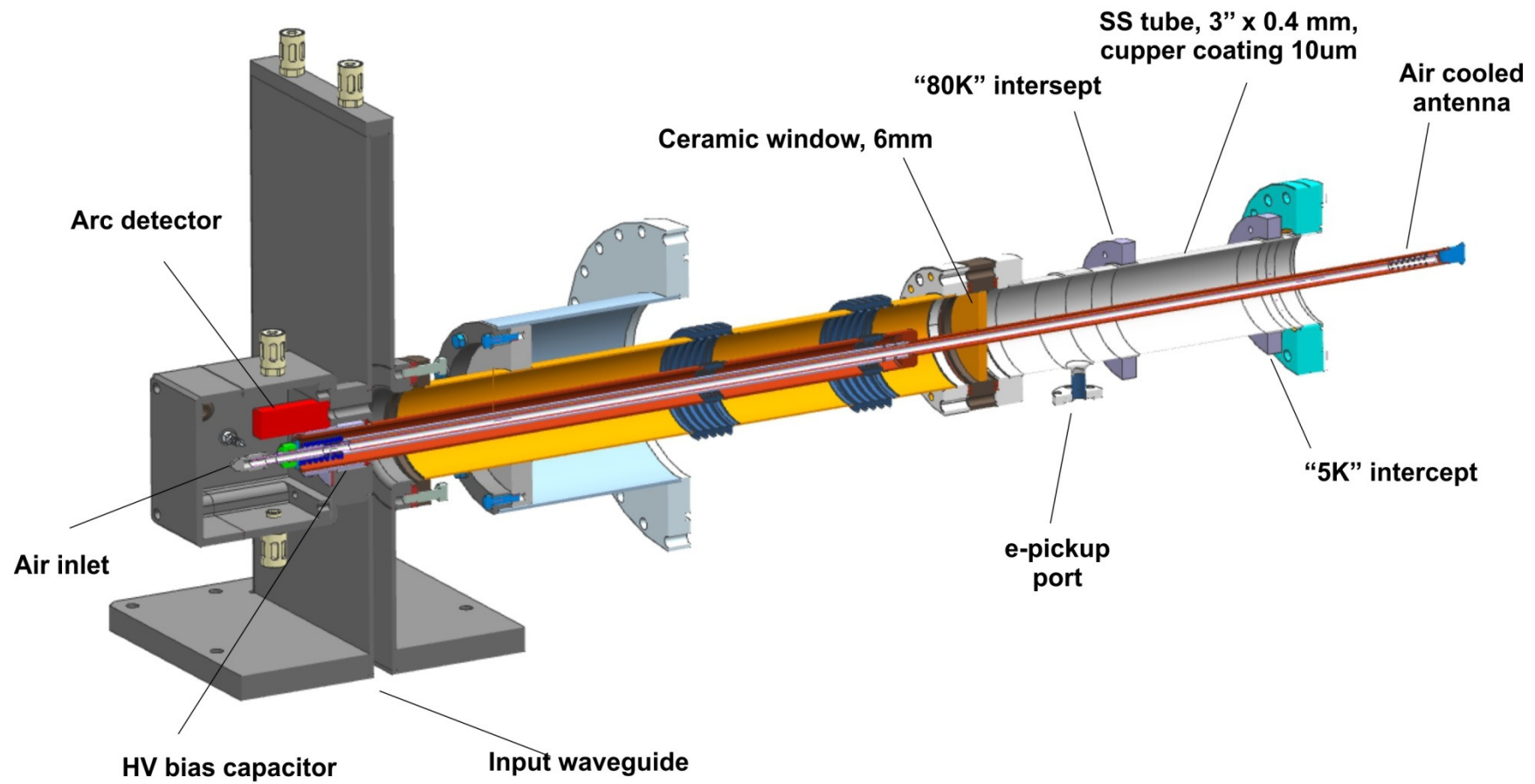
## Design approach:

- Simplest vacuum part, without bellows and, if possible, without copper coating.
- HV bias for multifactor suppression.
- High impedance to reduce losses in outer conductor (connected to 2K) and move multipactor zone to higher power.
- Air cooling of antenna.
- Single window.
- Similar design for 325 MHz and 650 MHz coupler to use the same proven solutions and technology.

**Based on this approach 325 MHz and 650 MHz couplers were designed:**



## Current structure of 650 MHz coupler



**Since that time two new ideas appeared:**

1. How to avoid copper coating.
2. How to make double window.

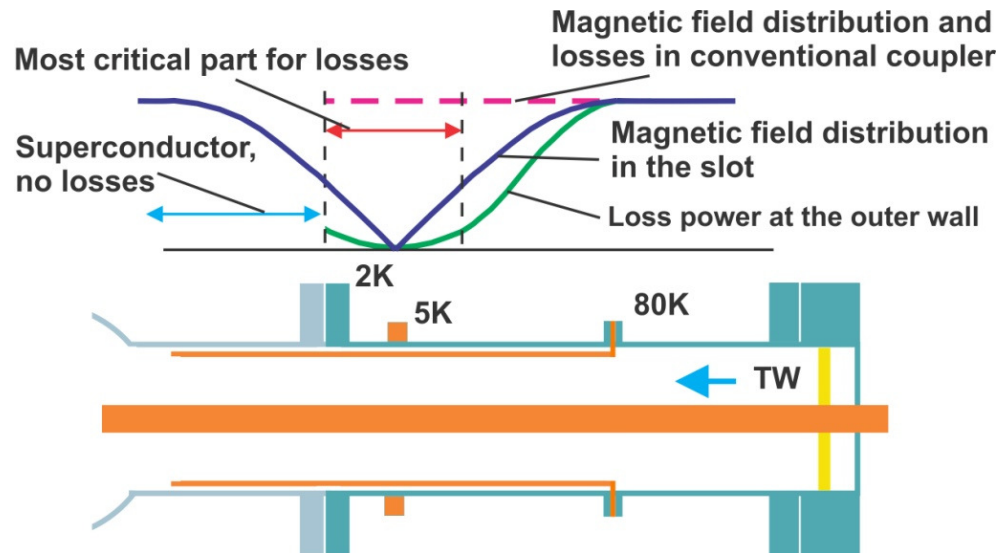
For 50 -100 kW, 650 MHz coupler, a pure stainless steel is not solution – too big RF losses. SS has to be coated with thin layer of copper.

**But copper coating has several drawbacks:**

1. Copper coating is not stable sometimes. Couple of times the copper flakes were found in 1.3 GHz cavities.
2. Coated copper has a lower RRR than ingot copper usually.
3. Copper increases the thermo-conductivity of structure. It increases static cryogenic load.

## How to avoid the copper coating? - Use copper shield for SS.

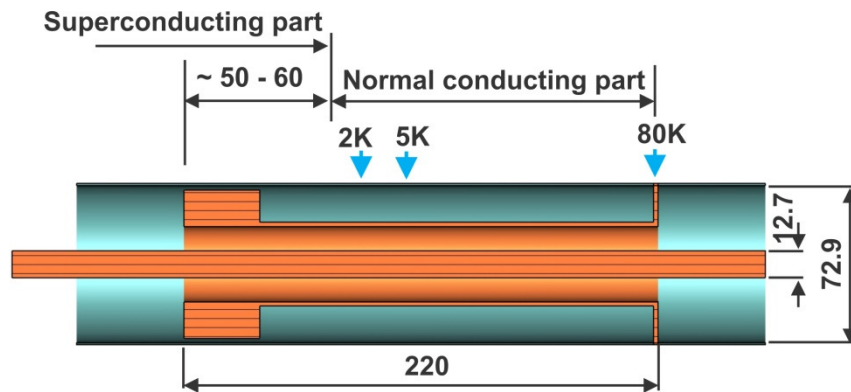
Idea started from this simpler geometry:



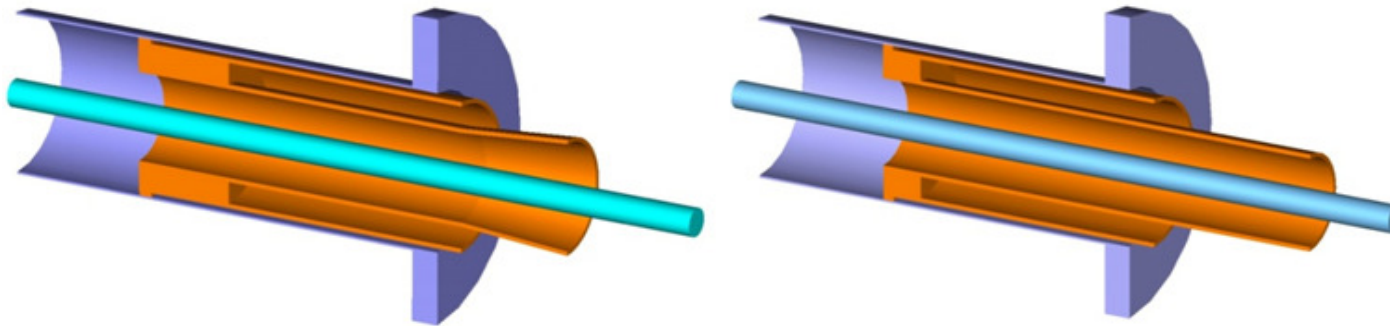
Coupler has a better performance then coupler with copper coating:

~ 0.7 power flow to 2K and ~ 0.8 power flow to 5K comparable to conventional coupler.

Performances are even better for these geometries:



Dynamic losses at 2 K are **50 times** smaller than for conventional copper coated coupler.

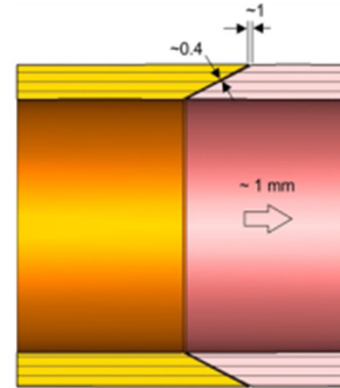
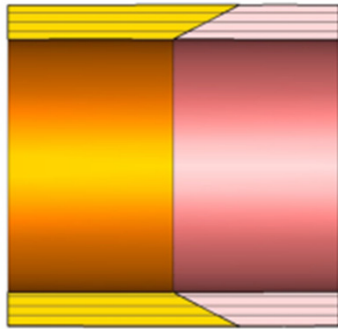


Fields are **zero** in slot. There are no dynamic losses at 2K and 5K at all.

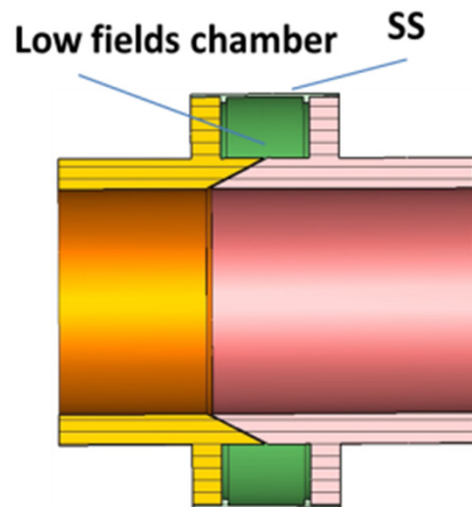


## Modification of idea:

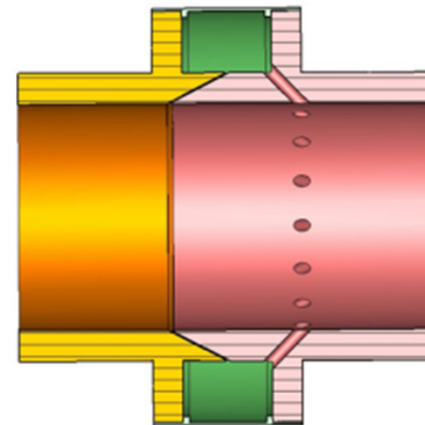
Idea:



No thermal contact  
between copper parts

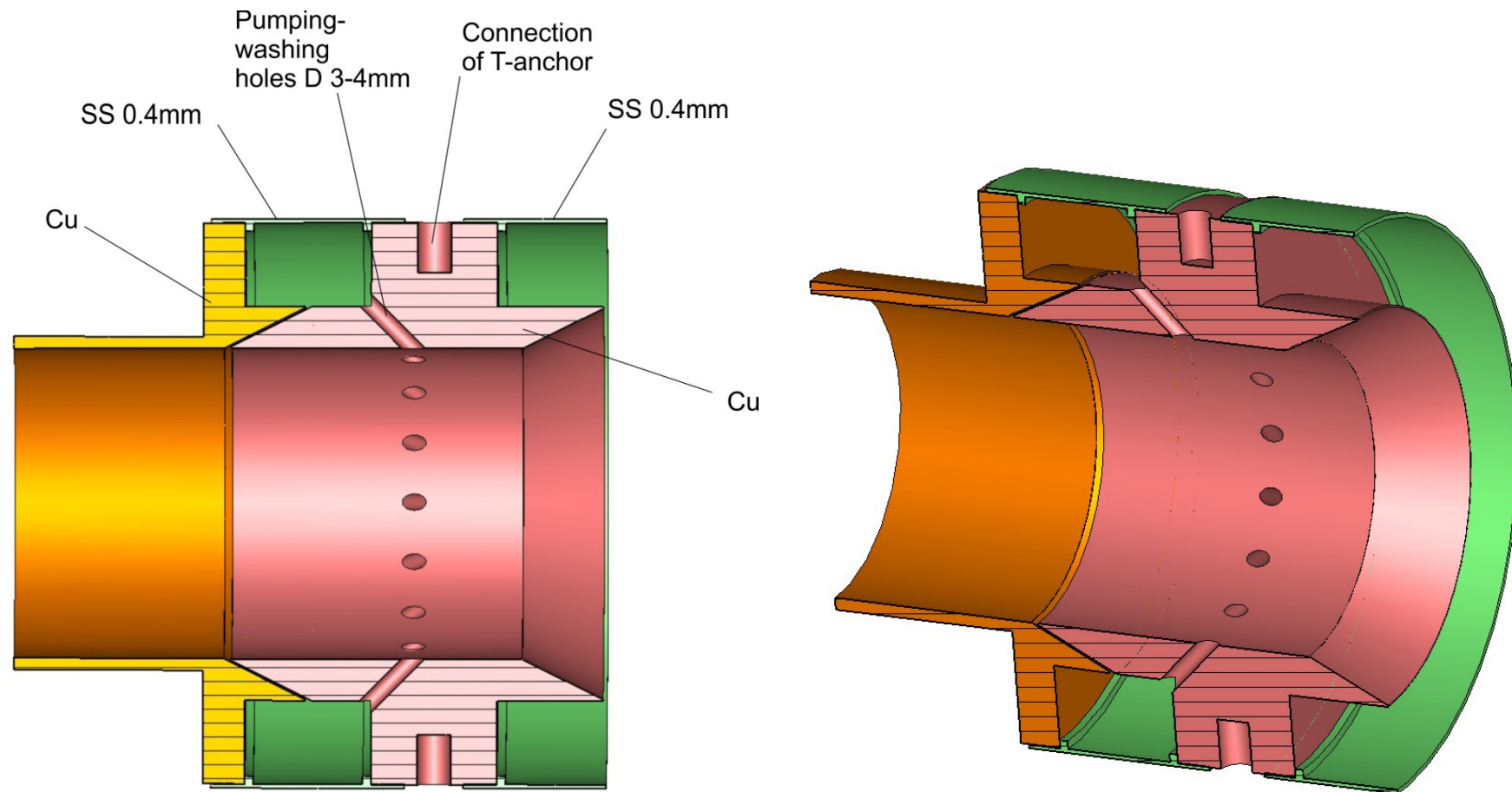


Heat flows through SS only,  
RF loss in SS < loss in Cu



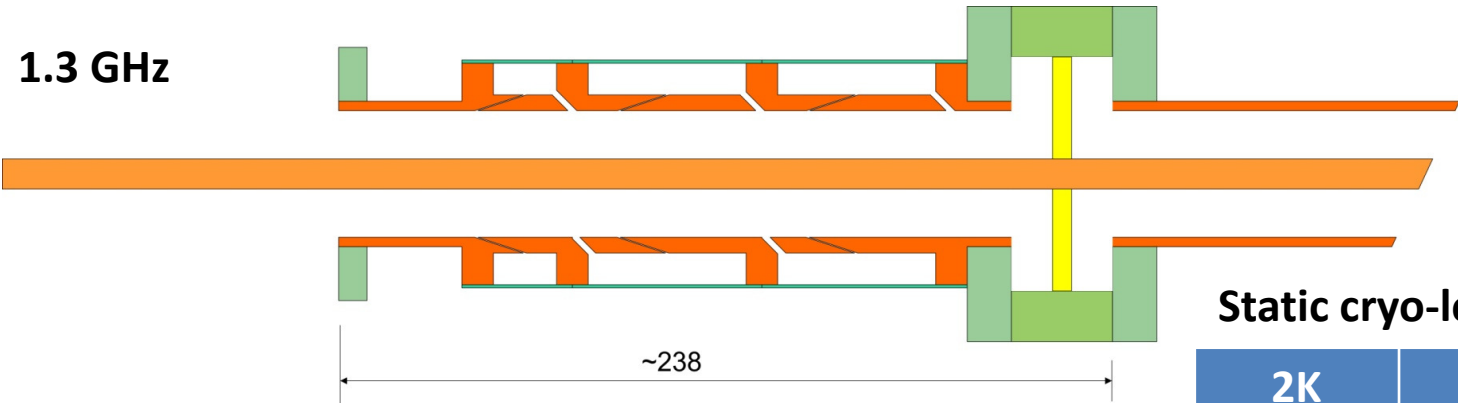
With some combinations of dimensions of slot and chamber:

- 1) RF reflections < -35 dB
- 2) H-field at SS surface < 0.25 of H-field at Cu surface (losses at SS will be < losses at Cu)



Possible configurations of 1.3 GHz and 650 MHz were presented to TD experts (cleaning and assembling):

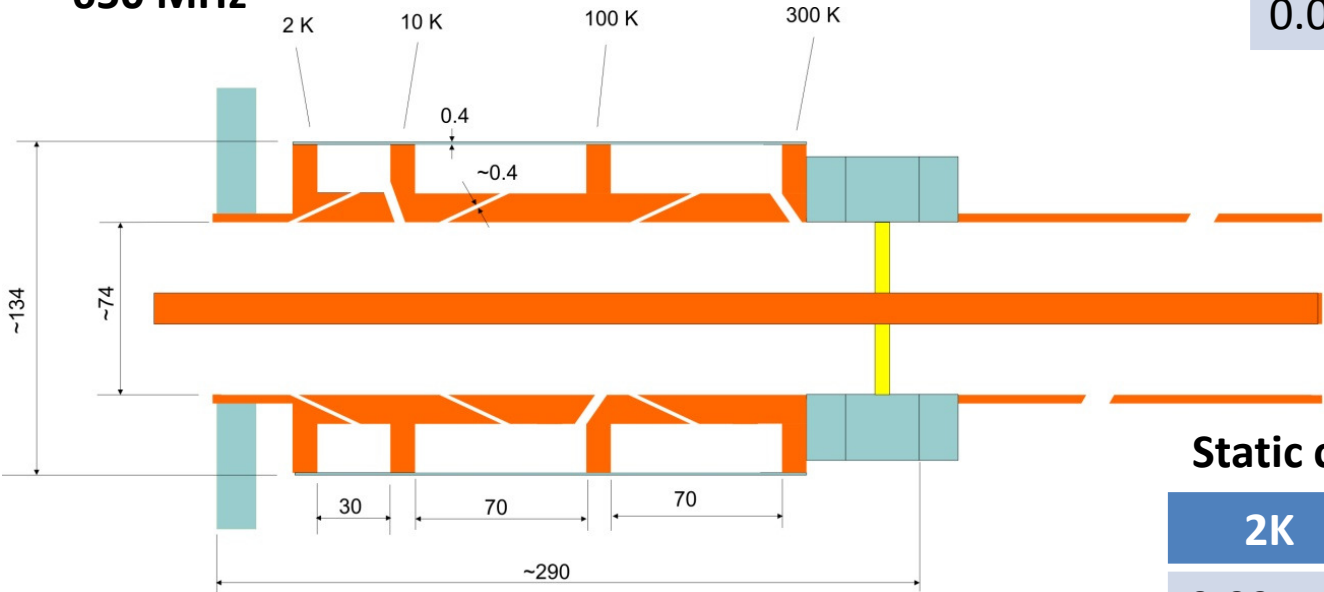
1.3 GHz



Static cryo-loading:

2K	10K	100K
0.017 W	0.90 W	3.2 W

650 MHz

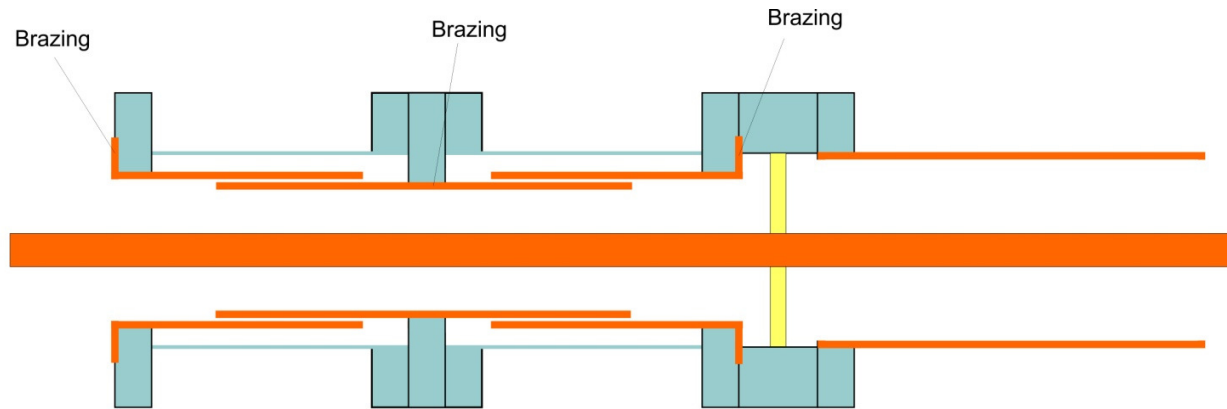


Static cryo-loads:

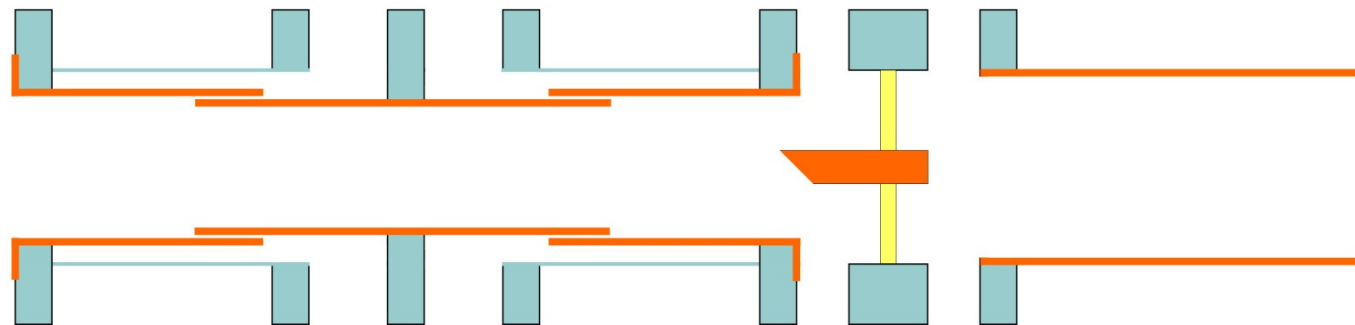
2K	10K	100K
0.021 W	1.25 W	4.8 W

Conclusion was: “it is difficult to clean (re-clean) closed chambers”.

Now we are proposing the dismountable configuration. It can be cleaned:

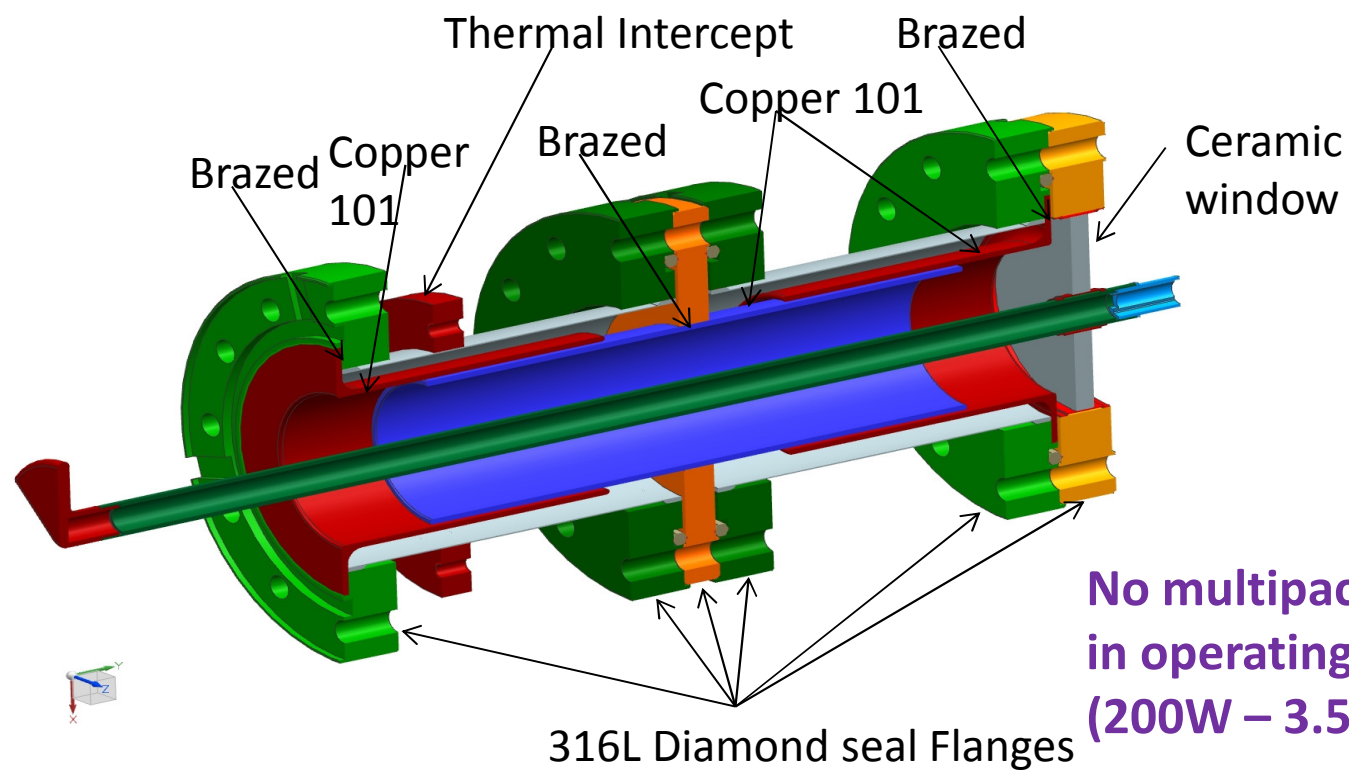
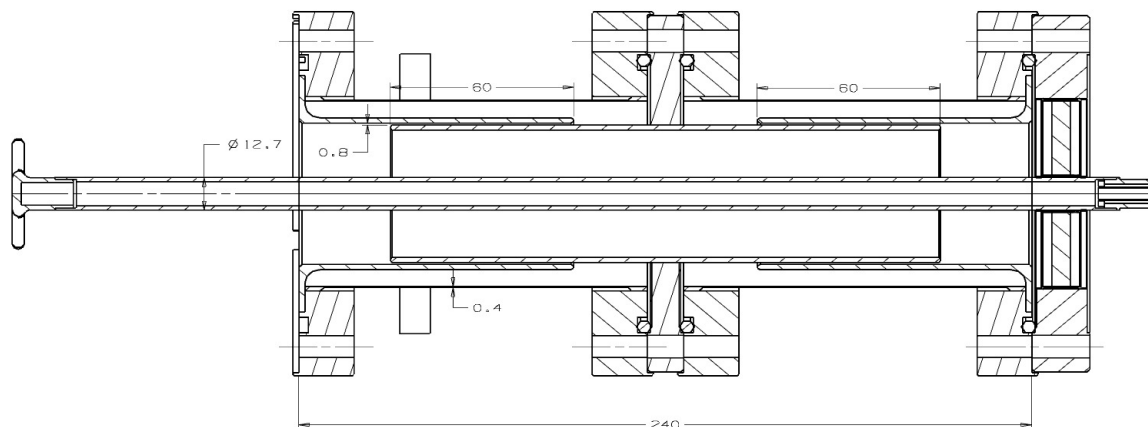


**Parts:**

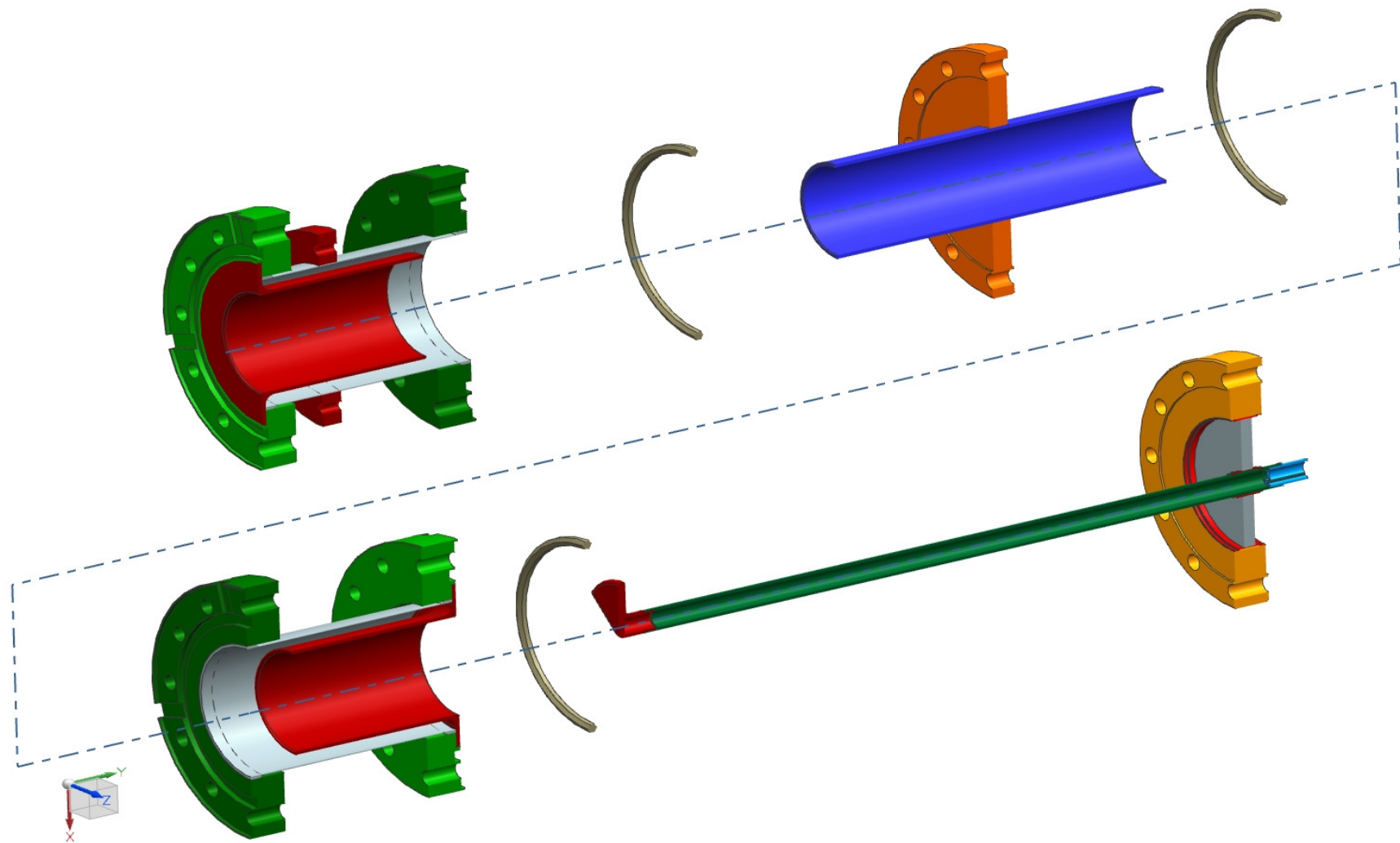


**Pro:** dismountable

**Con:** bigger number of flange



# Exploded view



**We hope to make two version of 650 MHz coupler for testing:  
with copper coating and with copper shielding.  
These parts will be interchangeable.**

# Double window.

We still have no solid answer how many windows coupler should have.

Single window and two windows have their own advantages and drawbacks.

## Two windows

### Pros:

more reliable

### Cons:

It is very difficult to provide antenna cooling for high power couplers (50 kW-100 kW).

It is necessary to mount a vacuum tight connection with cooling channels in antenna size area ( $\sim 0.5''$ - $1''$ ).

It is not clear how to detect reliably a possible crack of inner window for conventional two-window couplers. Vacuum is at both sides (window is cold, He has a low electric strength, good thermo-conductivity). Cold cavity works like a pump. It will be difficult to detect a leak. With small crack the window can RF operate without any sign of crack.

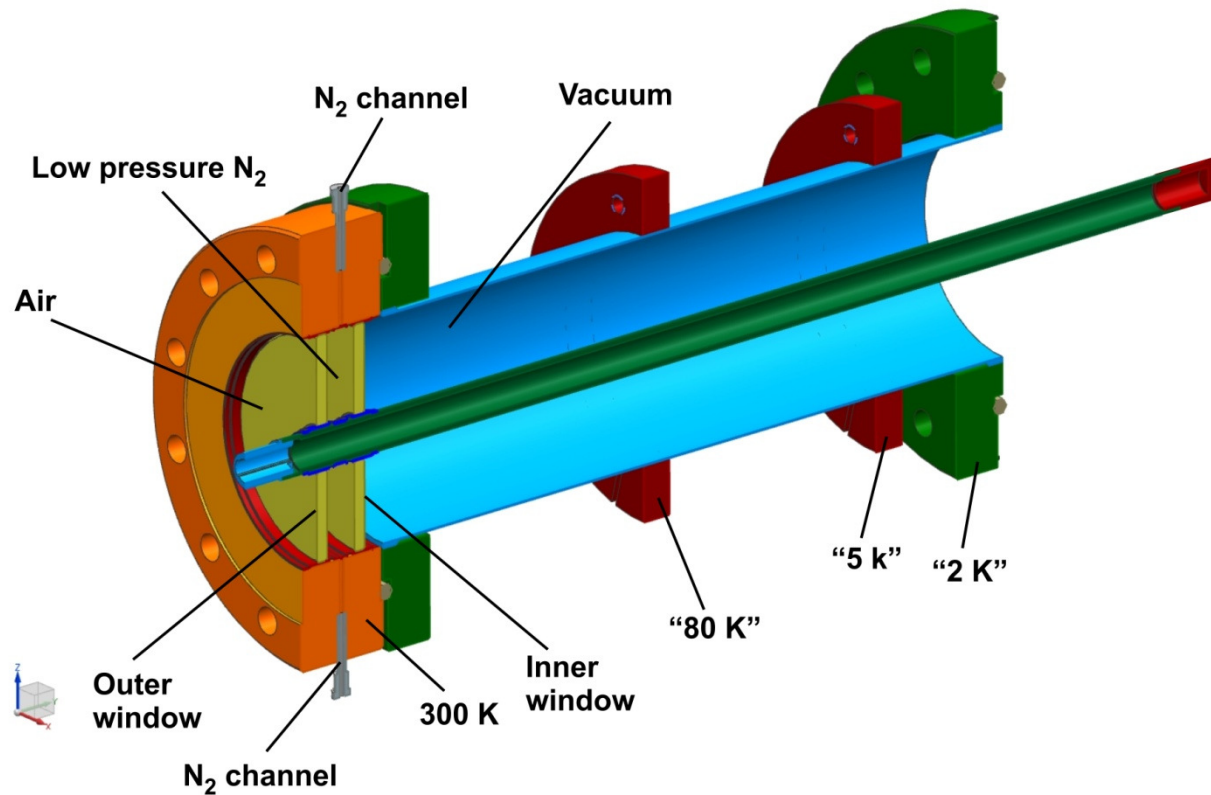


**Singe window:**

**Pros:** No cons of two windows

**Cons:** Less reliable.

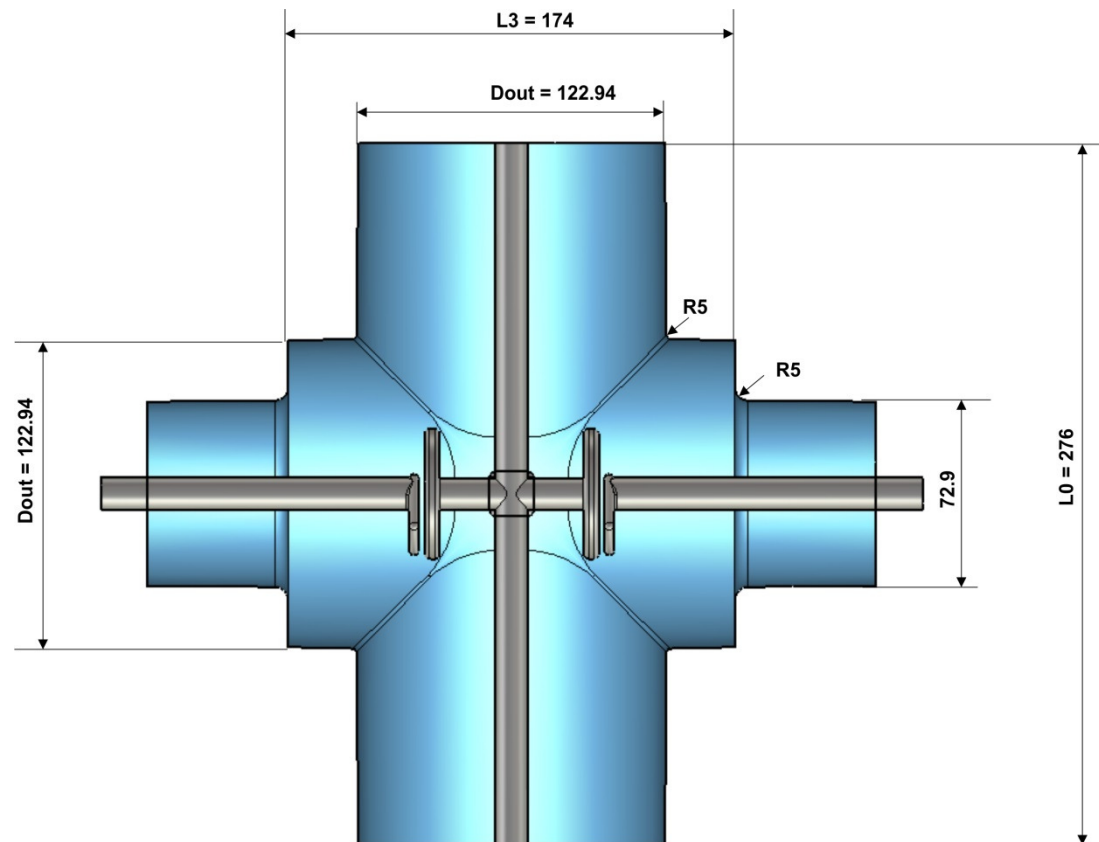
It seems there is solution which combines pros of both approaches: Leonardo suggested to place two windows close to each other as much as possible and use it as one unite. Both window is warm, we can place  $N_2$  between windows. In case of big crack of inner window some amount of  $N_2$  will come to accelerator,  $\sim 50 \text{ cm}^3$ , 0.06g,  $\sim 5e-4 \text{ bar}$  ( $\sim 5e-5 \text{ bar}$  in cryomodule). Hopefully it is not fatal to accelerator and  $N_2$  will not reduce performance of cavity (A. Romanenko).



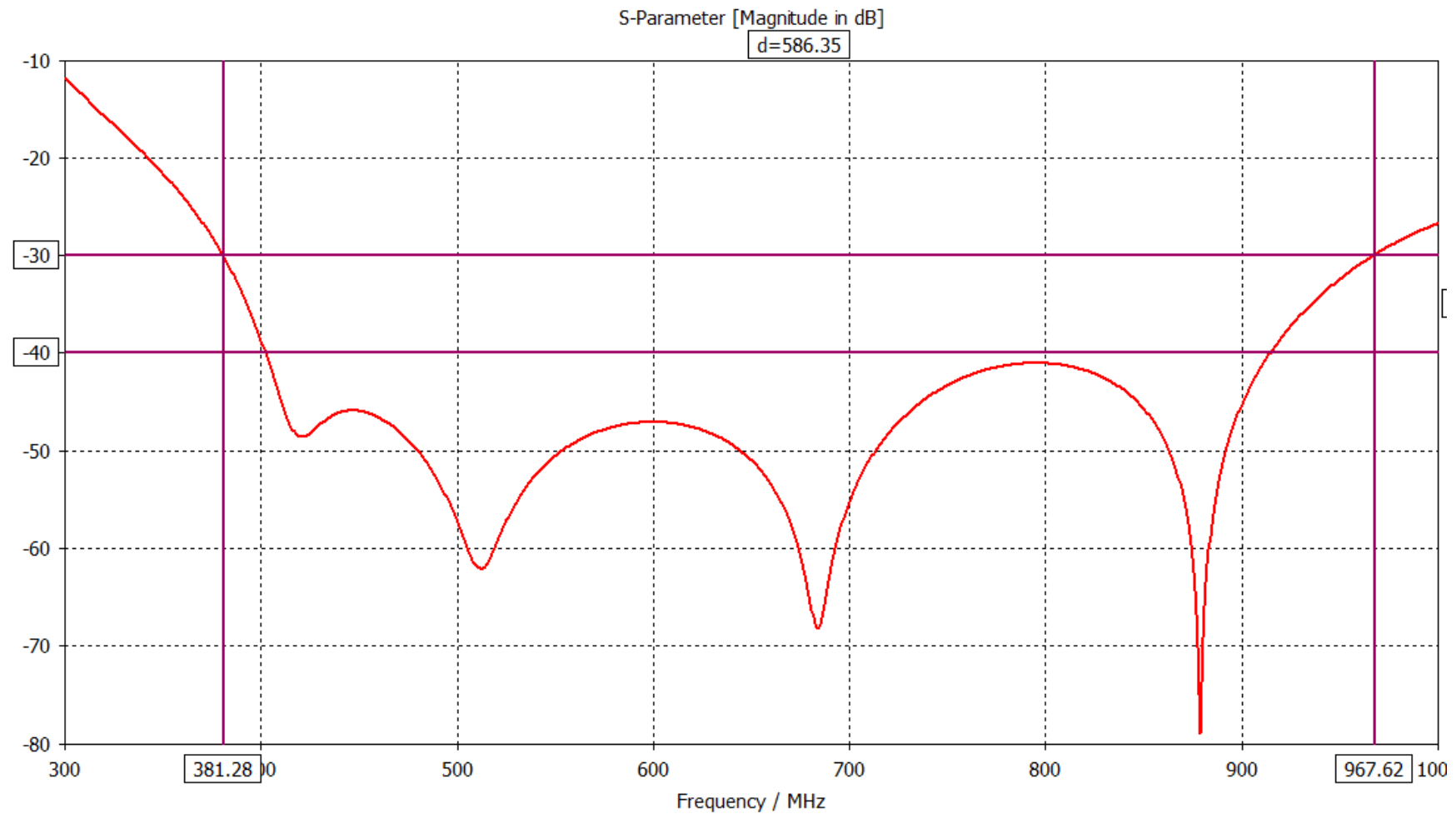
### Two close positioned windows.

- ☐ Advantages: reliability as two windows, compact as single window.
- ☐ Appearance of ceramic cracks can be detected: increasing pressure in cavity indicates of crack in inner window, increasing pressure between windows indicates of crack in outer window.
- ☐ Any one crack is not fatal for accelerator.

Interesting solution was found for test cavity for 650 MHz coupler testing: compact (not expansive) and extremely wideband (not sensitive to geometrical sizes).  
Sizes was chosen to avoid multipactor.



## Pass-band of 650 MHz test cavity:



~580 MHz at -30 dB !